It is seen that Boston's (4) and Fannin's (5) data are very near each other below ca. 350 °C and both data sets are slightly higher (ca. 0.2%) than our results in that range.

In the range 350-525 °C, outside the range of validity of any expressions of the literature it is seen that Fannin's (5) equation comes guite close to our measurements and that Boston's (4) and Sato's (7) extrapolated equations give too low and too high densities, respectively. Even around 600 °C Fannin's equation (5) reproduces our measurements within 0.5%.

At high temperatures (where Sato's equation (7) has its validity range) we note that our measurements fall in between Sato's and Fannin's extrapolated data. Sato's equation seems to give results which are 0.6% too high. (The precision of his equation is claimed to be $\pm 0.3\%$.)

Conclusion

Our expression for the density of molten NaAICI₄ as a function of temperature (model 4) deviates from the best data in the literature by less than 0.3%. Fannin's expression in the AICl₃-rich (acidic) range of the NaCl-AICl₃ system is probably very accurate (within 0.3%) and can presumably be extrapolated safely to higher temperatures (at least this is the case for the equimolar NaAlCl₄ composition). Sato's expression seems to give too high densities (0.6%) at least for the equimolar NaAICI₄ composition, perhaps due to the volatility of AICI₃ at high temperatures.

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Registry No. NaAlCl, 7784-16-9.

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Density of Sodium Tetrachloroaluminate Melts Containing Aluminum Chlorosulfides

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Liquid densities were measured for NaCi-AiCi₃ melts into which aluminum and sulfur in the molar ratio 2:3 had been dissolved. The densities were fitted by a polynomial function of temperature (range ca. 175 \leq t \leq 350 °C) and composition (ranges ca. 0.48 $\leq X_{\text{NaCl}} \leq$ 0.52 and 0 \leq $X_{Al_2S_3} \leq 0.04$).

Introduction

Recently it has been shown (1) that aluminum metal and elemental sulfur react in alkali tetrachloroaluminate melts forming aluminum chlorosulfides. These melts are colorless concentrated solutions, possibly containing solute ions like $[AI_n S_{n-1} CI_{2n+2}]^{n-1}$ and $[AI_n S_{n-1} CI_{2n+2-m}]^{(n-m)-1}$ $(n \ge 3$ and m < n). Such melts are of considerable interest, as they are formed during discharge of new galvanic cells based on the AI/S couple and a NaAlCl₄ electrolyte (2, 3).

The purpose of the present work was to determine an analytical expression for the densities of these melts, which are required for the calculation of solute concentrations and for estimations of battery weights. There are no previous measurements of densities of such solutions. In ref 1 we had to assume that the density of the solutions was approximately that of the NaCI-AlCI₃ solvent, which is known quite accurately (4-6).

Experimental Section

The densities were determined by the automated float method (7) (see also preceding paper (6)). NaCl and AlCl₃ of high purity were used (6). The aluminum consisted of carefully cleaned thin wires (Baker Analyzed Reagent, containing less than 0.05% Fe, 0.02% Cu, 0.05% Si, and 0.01% Ti, by weight). Sulfur of high purity was distilled before use. The chemicals were added in a dry glovebox to the quartz measuring cells which were sealed under vacuum and preequilibrated in a rocking furnace at ca. 300 °C for several days (until completion of reaction, characterized by the absence of aluminum metal and elemental sulfur).

Results and Discussion

The density as a function of temperature was measured for the nine compositions shown in Table I and in Figure 1. The aluminum and sulfur were weighed such that the molar ratio was as near to 2:3 as possible (the excess of either AI or S is indicated in Table I but ignored in the calculations of the mole fraction $X_{Al_{a}S_{a}}$).

The experimental "float" densities and the corresponding temperatures are given in Table II. After experiment 4-2 the floats were checked for etching by the melt during the five experimental runs, 3-0-4-2. On the average the densities of the floats decreased by 0.04%. This means that the accuracy

Table I.	Composition of the	Nine Experimental	l Melts Used for the Den	sity Determinations
				•

	initial composition, mmol ^a			mole fraction ^b				
expt no.	NaCl	AlCl ₃	"Al ₂ S ₃ "	total	X _{NaCl}	X _{AlCl} ,	$X_{Al_2S_3}$	excess of
1-0	145.96,	145.97	0	291.93,	0.5000	0.5000	0	
1-1 ^c	169.88	145.97	11.967	327.83	0.5182	0.4453	0.0365	0.021 mmol of S
1-2	169.88	165.98	11.967	347.84	0.4884	0.4772	0.0344	0.021 mmol of S
3-0	91.65	91.65	0	183.31	0.5000	0.5000	0	
3-1	92.40	91.65	0.384	184.44	0.5010	0.4969	0.0021	0.015 mmol of A1
4-0	102.82	99.30	2.605	204.73 ₈	0.5022	0.4851	0.0127	0.002 mmol of Al
4-1	107.51	99.30	5.156	211.97	0.5072	0.4685	0.0243	0.018 mmol of S
4-2	111.972	99.30	7.809	219.08_{7}	0.5111	0.4533	0.0356	0.483 mmol of S
5-0	125.46	136.06 _s	0	261.52	0.4797	0.5203	0	

^a 1 mmol = 10^{-3} mol. ^b X_{NaCl} = mol of NaCl/(mol of NaCl + AlCl₃ + Al₂S₃), etc. ^c I.e., cell no. 1, with addition no. 1.

Table II. Experimental Densities and Temperatures^a of the Molten NaCl-AlCl₃-Al₂S₃ System and for Comparison Densities Predicted from Table IV, Model 1

				density c	of floats, g cm ⁻³	predicted density
expt no.	X_{NaCl}	$X_{Al_2S_3}$	measd temp (SD), ^b °C	at 20 °C	at measd temp	(model 1), g cm ⁻³
1-0	0.5000	0.0000	165.6 (10) ^c	1.7096	1.7091	1.6998
1-0	0.5000	0.0000	299.8 (9)	1.6004	1.5996	1.6008
1-0	0.5000	0.0000	409.0 (10)	1.5181	1.5171	1.5202
1-0	0.5000	0.0000	511.5 (13)	1.4411	1.4399	1.4445
1-0	0.5000	0.0000	594.2 (15)	1.3823	1.3810	1.3834
1-1	0.5182	0.0365	220.8 (8)	1.7096	1.7090	1.7121
1-1	0.5182	0.0365	377.1 (8)	1.6004	1.5995	1.5968
1-1	0.5182	0.0365	500.6 (9)	1.5181	1.5169	1.5056
1-2	0.4884	0.0344	205.7 (11)	1.7906	1.7090	1.7068
1-2	0.4884	0.0344	350.6 (14)	1.6004	1.5995	1.5999
1-2	0.4884	0.0344	472.2 (20)	1.5181	1.5169	1.5101
3-0	0.5000	0.0000	195.4 (8)	1.6810	1.6805	1.6778
3-0	0.5000	0.0000	231.6 (9)	1.6538	1.6532	1.6511
3-0	0.5000	0.0000	245.3 (11)	1.6420	1.6413	1.6410
3-0	0.5000	0.0000	266.4 (10)	1.6257	1.6250	1.6254
3-1	0.5010	0.0021	198.6 (8)	1.6810	1.6805	1.6784
3-1	0.5010	0.0021	234.8 (9)	1.6538	1.6532	1.6517
3-1	0.5010	0.0021	249.2 (11)	1.6420	1.6413	1.6410
3-1	0.5010	0.0021	270.2 (10)	1.6257	1.6250	1.6255
4-0	0.5022	0.0127	175.6 (7)	1.7124	1.7120	1.7083
4-0	0.5022	0.0127	214.5 (10)	1.6810	1.6805	1.6796
4-0	0.5022	0.0127	251.0 (10)	1.6538	1.6531	1.6527
4-0	0.5022	0.0127	265.4 (12)	1.6420	1.6413	1.6420
4-0	0.5022	0.0127	287.4 (11)	1.6257	1.6250	1.6258
4-1	0.5072	0.0243	192.5 (7)	1.7124	1.7119	1.7119
4-1	0.5072	0.0243	232.6 (11)	1.6810	1.6804	1.6823
4-1	0.5072	0.0243	270.6 (12)	1.6538	1.6531	1.6543
4-1	0.5072	0.0243	285.2 (13)	1.6420	1.6412	1.6435
4-1	0.5072	0.0243	308.1 (12)	1.6257	1.6249	1.6266
4-2	0.5111	0.0356	209.2 (8)	1.7124^{d}	1.7119 ^d	1.7150
4-2	0.5111	0.0356	249.8 (11)	1.6810^{d}	1.6804^{d}	1.6851
4-2	0.5111	0.0356	289.5 (12)	1.6538^{d}	1.6530^{d}	1.6558
4-2	0.5111	0.0356	304.8 (14)	1.6420^{d}	1.6411 ^d	1.6445
4-2	0.5111	0.0356	328.2 (12)	1.6257	1.6249	1.6272
5-0	0.4797	0.0000	183.8 (8)	1.6827	1.6823	1.6812
5-0	0.4797	0.0000	193.8 (9)	1.6750	1.6745	1.6738
5-0	0.4797	0.0000	219.0 (10)	1.6529	1.6524	1.6552
5-0	0.4797	0.0000	258.8 (11)	1.6214	1.6208	1.6258

^a Temperature scan rates: 10-50 °C h⁻¹. ^b SD = standard deviation. ^c I.e., 165.6 ± 1.0 . ^d After the experiment 4-2, the densities of four floats were remeasured; at 20 °C they gave 1.7118, 1.6806, 1.6530, and 1.6410 g cm⁻³ and after correction for expansion at the measured temperatures 1.7112, 1.6799, 1.6523, and 1.6402 g cm⁻³.

of the densities must be taken to be not better than ± 0.001 g cm⁻³. The etching probably occurred on all floats and also on the inside surfaces of the quartz cells. Hence, the melts must contain small amounts of dissolved SiO₂, presumably of the order of 0.05% by weight, assuming uniform etching of all internal quartz surfaces. In experiments 1-1 and 1-2 the etching was probably worse since these cells have been heated to higher temperatures. These cells probably were saturated with oxides according to the reactions (8-10) SiO₂(s) \rightleftharpoons SiO₂(dissolved), SiO₂(s) \rightleftharpoons 4/₃AlCl₃(l) \rightleftharpoons 2/₃Al₂O₃(dissolved) + SiCl₄(g), Al₂O₃(s) \rightleftharpoons Al₂O₃(dissolved), but the solubility of silica and alumina is believed to be rather small so that the density

data obtained should still be close to the data valid for the pure NaCl-AlCl₃-Al₂S₃ system.

The density as a function of temperature for each experiment is plotted in Figure 2. As can be seen, there is in all cases a largely linear dependence. In Table III the obtained densities for each composition are given by the equation

$$\rho = A(X_{\text{NaCl}}, X_{\text{Al}_2\text{S}_3}) - B(X_{\text{NaCl}}, X_{\text{Al}_2\text{S}_3})(t - 175)$$
(1)

where ρ is the density in g cm⁻³, A and B are fitting parameters which depend on composition, and t is the temperature in °C. The uncertainty in the A parameter is smaller when the temperature dependence is based on 175 °C than when developed



Figure 1. Graphical representation of the experimental compositions covered in this work.



Figure 2. Densties of the nine compositions of the NaCl-AlCl3-Al2S3 system as function of temperature: experiments (A) 5-0, (B) 3-0, (C) 1-0, (D) 3-1, (E) 4-0, (F) 4-1, (G) 1-2, (H) 4-2, and (I) 1-1.

from the usual 0 °C. This is, of course, of importance when the dependence on composition is being investigated.

A convenient way to represent the results is to combine the data obtained at different temperatures and compositions into one empirical equation which fits the observations as closely as possible.

Using standard least-squares regression methods (11), we tried general polynomial expressions like

$$\rho = a + bt + ct^{2} + dX_{\text{NaCi}} + eX_{\text{NaCi}}^{2} + fX_{\text{Al}_{2}\text{S}_{3}} + gX_{\text{Al}_{2}\text{S}_{3}}^{2}$$
(2)

Analysis of regression models using different analytical equations like eq 2 to fit the data of Table II showed that terms in t^2 and $X_{Al_2S_3}^2$ were of no significance. The two most satisfactory analytical expressions and the corresponding parame-

Table III. Linear Density Equations of the Molten NaCl-AlCl,-Al,S, Experiments^a Obtained by Least-Squares **Regression Analysis**

		<i>B</i> , ^b g		
expt no.	<i>A</i> , ^{<i>b</i>} g cm ⁻³	cm ⁻³ °C ⁻¹	r ² ^c	SD, g cm ⁻³
1-0	$1.6984 (29)^d$	7.65 (10)	0.9994	0.0036
1-1	1.7398 (20)	6.87 (9)	0.9998	0.0017
1-2	1.7296 (43)	7.22 (21)	0.9991	0.0004
3-0	1.6968 (8)	7.83 (12)	0.9995	0.0006
3-1	1.6990 (6)	7.76 (9)	0.9997	0.0005
4-0	1.7120 (5)	7.77(7)	0.9997	0.0006
4-1	1.7245 (7)	7.52 (8)	0.9997	0.0007
4-2	1.7361 (10)	7.29 (9)	0.9995	0.0009
5-0	1.6895 (6)	8.24 (12)	0.9995	0.0007

^a For the measured temperature ranges. ^b $\rho =$

 $A(X_{\text{NaCl}}, X_{\text{Al}_2S_3}) - [B(X_{\text{NaCl}}, X_{\text{Al}, S_3}) \times 10^{-4}](t - 175).$ $c r^2 = \text{coefficient of regression, defined as in ref 6.} d \text{ I.e.,}$ 1.6984 ± 0.0029 .

Table IV. Coefficients in the Empirical Polynomial^a for the Density of the Molten NaCl-AlCl₃-Al₂S₃ System^b

	model 1	model 2	
A	1.693 (1)	1.693 (1)	
В	7.38 (6)	7.38 (6)	
С	0.42 (8)	0.35 (7)	
D	7.9 (5.0)		
Ε	1.17 (5)	1.21 (5)	
SD, g cm ⁻³	0.0037	0.0038	
r^2	0.9977	0.9975	

^a $\rho = A - (B \times 10^{-4})(t - 175) + C(X_{\text{NaCl}} - 0.5) + D(X_{\text{NaCl}} - 0.5)^2 + EX_{\text{Al}_2S_3}$ in g cm⁻³, t in °C. ^b Temperature range 175-350 °C, X_{NaCl} range 0.48-0.52 and X_{Al₂S₃} range 0-0.04.

ters are shown in Table IV. The best expression, model 1, gives a slightly better fit but also has one parameter (D) more than model 2. The significance of D may be questioned but parameters A, B, C, and E are indispensable.

In order to test the validity of the expressions in Table IV, we compared predicted densities with the measurements on acidic and basic NaCl-AICl₃ melts by Fannin et al. (4) and Sato et al. (5) ($X_{Al_2S_3} = 0$). The predicted densities show variations in temperature and composition similar to the observations and are generally accurate to within 0.01 g cm⁻³ or better, inside the range of validity of our equation.

Registry No. NaAlCI, 7784-16-9; Al, 7429-90-5; S, 7704-34-9.

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